



Technical and radiological characterisation of fly ash and bottom ash from thermal power plant

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Abstract

Huge quantities of fly ash and bottom ash are generated from thermal power plants and it presents great concern for country, mainly due to the environmental effects. In this study, fly ashes and bottom ash were characterized from technical and radiological aspects. Health effect due to the activity of radionuclides ^{226}Ra , ^{232}Th and ^{40}K was estimated via radium equivalent activity (Raeq), external hazards index (H_{ex}), the external absorbed dose rate (D) and annual effective dose rate (EDR). The specific surface area ($40.25 \text{ m}^2 \text{ g}^{-1}$), particle density (1.88 g cm^{-3}) and LOI (23.49%) were typical for bottom ash. Siliceous fly ash contained 32% reactive silica. The annual effective dose rate for all ashes is $\leq 0.2 \text{ mSv y}^{-1}$. Both, fly ash and bottom ash present potential secondary raw materials to be used for building purposes as result of their technological and radiological assessment.

Keywords Fly ash · Bottom ash · Gamma spectrometry · Building materials

Introduction

Fly ash (FA) and bottom ash (BA) are the major industrial residues (waste/ by-products) formed with the production of electricity in thermal power plants. FA presents fine particulate residue resulting from the combustion of coal which is captured from fly gas and collected by electrostatic

precipitator. BA is heavier and harder to be carried out with fly gas and it is collected at the bottom of the boiler. The particles of BA are much coarser, angular and large sized (in range from sand to gravel size) with rough surface texture and gray color due to the presence of unburn carbon. BA possess high permeability, strength and compressibility which properties make BA promising material for civil engineering applications. Chemical composition of BA is similar to FA, (mainly composed of SiO_2 , Al_2O_3 , Fe_2O_3 , CaO and small amounts of magnesia, titania, etc.), but with greater content of unburned carbon. Fly ash particles are spherical and alkaline in nature [1–3].

The management of both ashes remains the global environmental problem. Significant amounts of ashes are already used in range of applications, but still there is need to address the potential reuse of ashes. Recent literature reports the application of FA in construction: as raw material in Portland cement clinker [4] and belite-sulfoaluminate clinkers [5], as pozzolanic addition in cement [6], concrete [6, 7], light weight aggregate [6], bricks [8], glass-ceramics [9] etc. Also, other uses are being developed, like adsorbents [6, 10], zeolites [11], macro and micro nutrients in agriculture [10]. Nowadays its potential utilization due to the new technologies is much wider in the sense of its

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green transformation. For instance, fly ash can be used as a source of carbon for the synthesis of nanomaterials (carbon nanotubes), aerogels, geopolymers and rare earth elements [12]. Bottom ash showed better capability to be used for geotechnical construction like in roadways, embankments and fill material [13], as constituent in belite-sulfoaluminate clinkers [14] and as micro filler in concrete [15], but also as constituent in Portland cement [16] glass-ceramics [17], ceramics [18], etc. According to European Coal Combustion Products Association [19] most of the coal combustion products (CCPs) produced are used in the construction industry, in civil engineering and as construction materials in underground mining (52.4 wt.%) or for restoration of open cast mines, quarries and pits (35.9 wt.%), fly ash (FA) in blended cements (11%) and cement raw material (26%) of 21 million tons and bottom ash (BA) in cements (10%) of 2.6 million tons.

The composition, morphology and size of particles, the nature of crystalline phases and glasses, unburned carbon, trace and heavy elements vary in fly ash and bottom ash, but the above mentioned variations influence on the behavior of ashes in their applications. On the other hand, coal ashes (fly ash and bottom ash) as industrial residues (waste and/or by-products) contain enriched concentrations of natural radionuclides considered as naturally occurring radioactive materials (NORM). According to the Council Directive 2013/59/EUROATOM, 2013, Article 75 [20], the referent level for indoor external exposure due to the gamma radiation emitted by building materials is 1 mSv y^{-1} . Also, the directive defines the activity concentration index for gamma radiation emitted by building materials—I as a conservative screening tool to identify building materials that may be of concern from a radiation protection point of view. NORM used in the final building material has to be assessed from a radiological point of view before it is used in standard practice.

This study presents part of the results of RIS ALiCE registry [21] developed for Al-containing secondary mineral residues (industrial and mine wastes/by-products) as a base for increased production of low CO_2 mineral binders, based on belite-sulfoaluminmate clinkers (BCSA) in ESEE region [22]. This work aimed to determine the technical and radiological characterization of the fly ash (fresh and landfilled/historical) and bottom ash from the thermal power plant REK Bitola, Republic of North Macedonia and to foresee the potential for their utilization. Thermal power plant REK Bitola is the main producer of energy in the Republic of North Macedonia participating with more than 80% of the total electricity production [23]. Annually, 1.5 million tons of fly ash are produced and only 120 000 tones are utilized as blended in cement [24]. Large quantities of fly ash and bottom ash remain on the surrounding of the thermal plant and the potential sustainable solutions are needed.

Experimental

Materials

The materials used in this research were obtained from the largest thermal power plant (REK Bitola) from Republic of North Macedonia. Three ashes were investigated: fresh fly ash (FA) sampled from electro filter, landfilled/historical fly ash (LFA) sampled from the open land field and bottom ash (BA) sampled from the bottom of the reactor.

Methods

Physical characterization

Particle size distribution (PSD) of the fly ash and bottom ash was dry measured by a laser scattering particle size distribution analyzer (HelosH4087 & RODOS). Ashes passed through the $200 \mu\text{m}$ sieve prior to the PSD analyses [25].

Moisture content was calculated by the relation: $\% \text{mc}_{\text{wb}} = (m_{\text{w}} - m_{\text{d}}/m_{\text{w}}) \times 100$, where mc_{wb} is expressed on a wet basis (where: m_{w} is the mass of the wet fly ash and m_{d} is the mass of dry fly ash). The particle density of ashes was determined by the pycnometer method [26] and bulk density according to JUSB.C8.023 standard [27].

The morphology of the ashes was investigated by scanning electron microscope (JEOL JSM 5500LV). The specific surface area (SSA) of the ashes was determined by BET method (Micromeritics ASAP-2020), by nitrogen adsorption measurements at 77 K.

Chemical and mineralogical composition

The chemical composition of fly ashes and bottom ash was carried out on fuse bead samples by x-ray fluorescence spectroscopy (ARL 9900 instrument). Reactive silicon dioxide (SiO_2) only at FA and loss of ignition (LOI) were determined according to the EN196-2 standard [28].

Trace elements (TE) and rare earth elements (REE) were determined by ICP-OES (Perkin Elmer Avio200 ICP-OES) instrument with S10 autosampler, MiraMIST nebulizer, glass baffled cyclonic spray chamber and lutetium as the internal standard. Sample preparation include grinding to under 1 mm and fusion with lithium metaborate (0.5 g sample + 1.16 g lithium metaborate + 0.05 g NH_4NO_3) at $1000 \text{ }^\circ\text{C}$ (1 h) in platinum crucible [29]. AMA 254 Advanced Mercury Analyzer was used for determination of mercury.

The mineralogical composition of ashes was determined by an X-ray diffractometer (PANalytical Empyrean). The internal wavelengths used were from copper anodes ($\lambda\text{CuK}\alpha 1 = 1.54 \text{ \AA}$, $\lambda\text{CuK}\alpha 2 = 1.54 \text{ \AA}$, $\lambda\text{CuK}\beta 1 = 1.39 \text{ \AA}$)

with a reflection transmission spinner configuration. Samples were ground in an agate mortar to a particle size below 0.063 mm. The ground powder was manually back-loaded into a circular sample holder (diameter 27 mm), data for each sample were collected from 4° to 70° (2θ). The X-ray tube worked at 45 kV and 40 mA and the samples were rotated during data collection at a revolution time of 2 s. Amount of amorphous phase and mineral phases were estimated by Rietveld refinement with the external standard method (pure corundum, Al₂O₃; NIST 6769) and PANalytical X'Pert High Score Plus diffraction software, using the structures for the phases from ICDD PDF 4 + 2016 RDB powder diffraction files.

Radiological characterization

Gamma-ray spectrometry Gamma spectrometry was employed for measuring the activity concentration of radionuclides in coal ashes. The ash samples were placed in PVC cylindrical containers six weeks prior to the measurements in order to reach the radioactive equilibrium.

Radiological analysis was performed according to the [30] employing a coaxial semiconductor high purity germanium (HPGe) detector (Canberra GC5019 with 50% relative efficiency and 1.8 keV resolution for ⁶⁰Co line at 1332 keV) associated with a standard high voltage supply and electronics units. Based on the obtained results for ²²⁶Ra, ²³²Th and ⁴⁰K activity concentration of ashes, the I-index was determined (considered as a screening tool for the radiological behaviour of ashes) and dose assessment was performed.

Activity concentration index (I-index) The index I was calculated, according to Eq. (1) [20].

$$I = C_{226\text{Ra}}/300 + C_{232\text{Th}}/200 + C_{40\text{K}}/3000 \quad (1)$$

where $C_{226\text{Ra}}$, $C_{232\text{Th}}$ and $C_{40\text{K}}$ are activity concentrations in Bq kg⁻¹ in the measured samples.

Dose assessment & radium equivalent activity & The external hazard index Radium equivalent activity, Ra_{eq} (Bq kg⁻¹), the external hazard index, H_{ex} (Bq kg⁻¹), total external absorbed gamma dose rate D (nGy h⁻¹) and annual effective dose rate EDR (mSv y⁻¹) were calculated in order to estimate the potential health effect of the ashes due to the exposure of the public to natural radioactivity.

The radium equivalent activity, Ra_{eq} , as a tool to limit the exposure to radiation, was calculated according to Eq. (2). It should be lower or equal to 370 Bq kg⁻¹ in order to limit the gamma dose from building materials to 1μSv y⁻¹ [31].

$$Ra_{eq} = C_{Ra} + 1.43 C_{Th} + 0.077 C_k \quad (2)$$

The external hazard index, H_{ex} , was calculated according to Eq. (3) and it reflects the external radiation hazard due to the emitted gamma radiation.

$$H_{ex} = (C_{Ra}/370) + (C_{Th}/259) + (C_K/4180) \quad (3)$$

The external terrestrial gamma radiation absorbed dose rate, D, in the air at a height of 1 m above ground level due to the presence of radionuclides ²²⁶Ra, ²³²Th and ⁴⁰K in fly ashes and bottom ash were calculated using Eq. (4) [31].

$$D = 0.462C_{Ra} + 0.604C_{Th} + 0.0417C_K \quad (4)$$

where 0.462, 0.604 and 0.0417 are conversion factors for ²²⁶Ra, ²³²Th and ⁴⁰K in (nGy h⁻¹)/(Bq kg⁻¹), respectively.

The annual outdoors effective dose rate, EDR, was calculated by Eq. (5) using a conversion coefficient of 0.7 Sv G⁻¹y⁻¹ to convert the absorbed dose in the air into the effective dose in the human body. This calculation takes into account that the people spend about 20% of the time outdoors (outdoor occupancy factor p is 0.2) and t is 8.760 h annual exposure time.

$$EDR(\text{mSv y}^{-1}) = D(\text{nGy h}^{-1}) \times t \times p (\text{h y}^{-1}) 0.7(\text{Sv G}^{-1}\text{y}^{-1}) 10^{-6} \quad (5)$$

Results and discussion

Physical characteristics of ashes

The particle size distribution curves of ashes are present in Figs. 1, 2 and 3. The mean diameter, D₅₀, for FA and LFA is 30.57 μm and 42 μm, respectively and 120 μm for BA (Table 1). BA contains higher amount of large particles in comparison to FA and LFA, as the curve is moved to the right side. The particle size distribution for fly ash samples is broader than for bottom ash. Namely, particles in the range of 50 to 200 μm in diameter are accounted for the most of the sample, while in FA and LFA most particles are in the range 10 and 110 μm. It is evident that all ashes have unimodal particle size distribution.

The obtained data for specific surface area, moisture content, particle density and bulk density, presented in Table 1 shows that a significantly higher specific surface area has bottom ash (40.25 m² g⁻¹) due to the presence of unburned coal particles. Moisture content is expected to be higher in the LFA and BA due to the weathering of landfilled fly ash and the production process of bottom ash. Particle density and bulk density is the highest for LFA, while is the lowest for BA. Bottom ash is known to have low particle density and low bulk density and is therefore commonly used as a lightweight aggregate or light fill material [1–3].

Fig. 1 Particle size distribution of FA

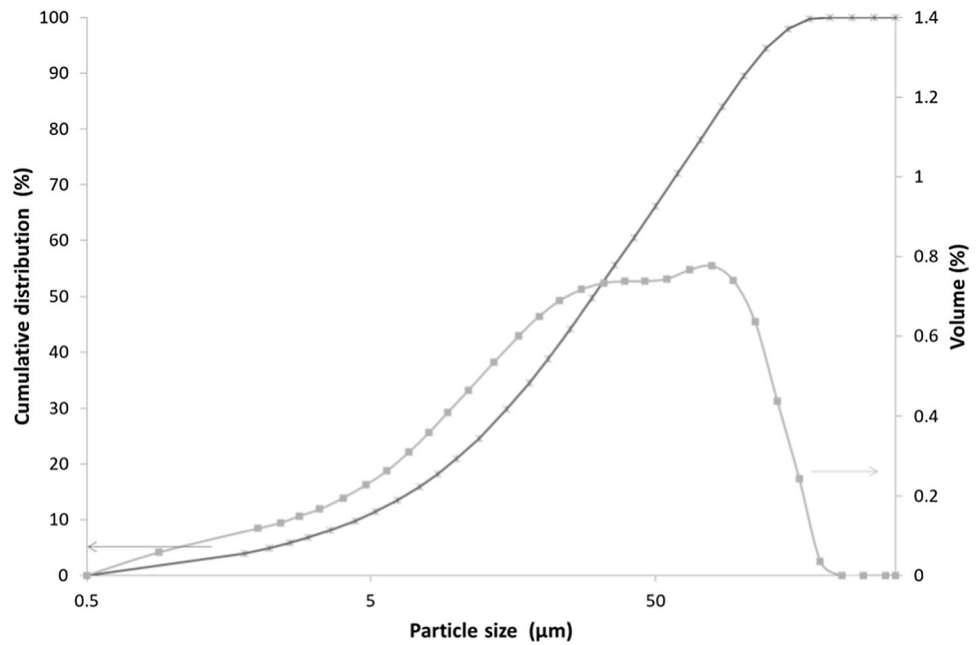
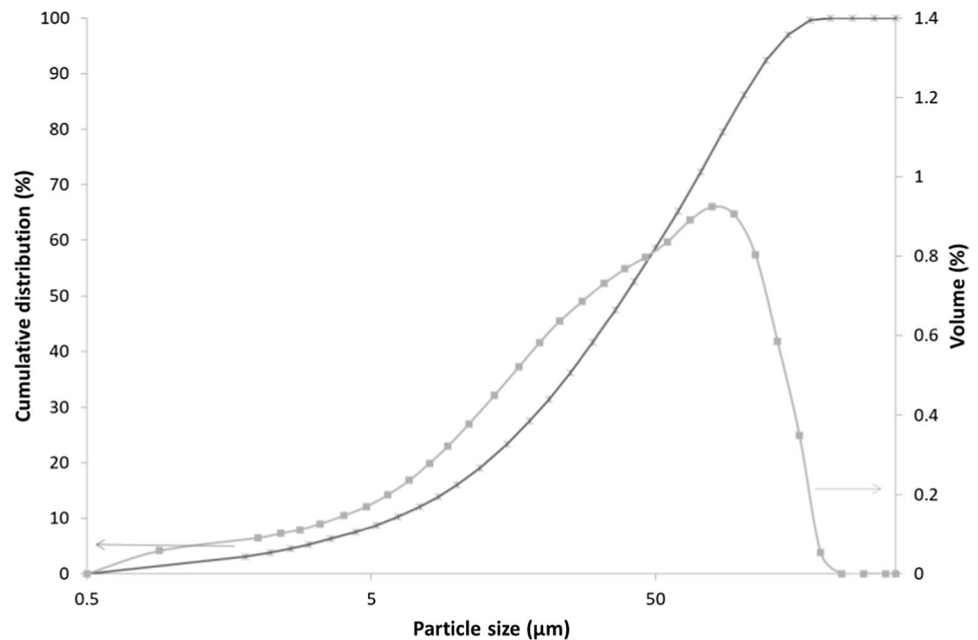


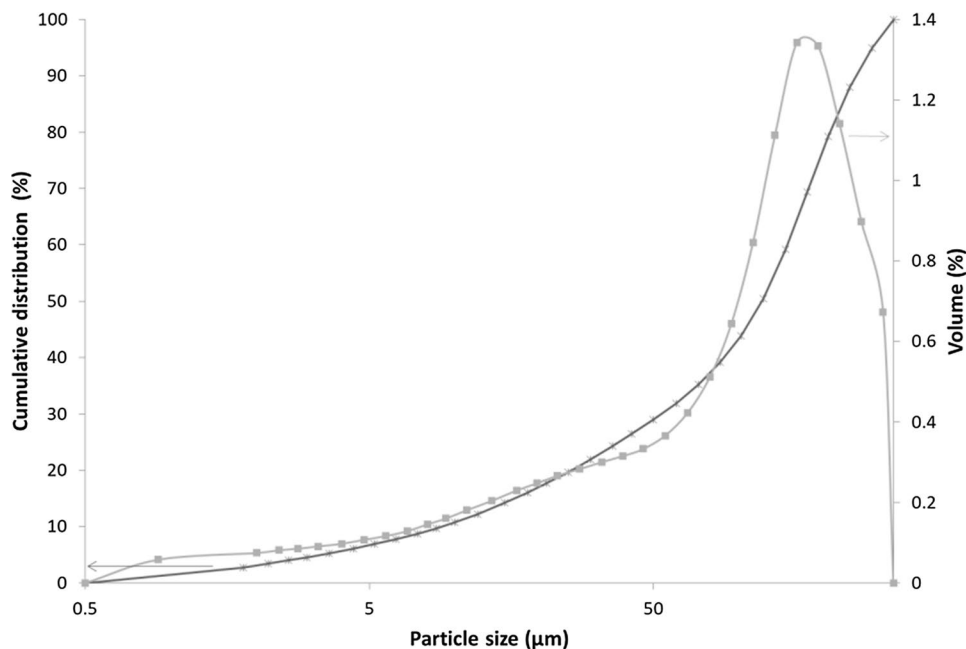
Fig. 2 Particle size distribution of LFA



The morphologies of fly ashes FA and LFA are presented in Fig. 4. It is evident heterogenic distribution of particles, the presence of typical fly ash cenospheres with dimensions from 2 to 20 μm , particles with a smooth surface, but irregular geometry and coarse particles mainly composed of unburned carbon. Much coarser particles with irregular geometry and sharp edges are observed in bottom ash (Fig. 4c). Bigger porous particles originate from coal are more widespread in the bottom ash, confirmed by the chemical composition (Table 2). Similar morphology observation for both ashes has also been noticed in [2].

Chemical and mineralogical composition of ashes

The chemical composition of ashes is influenced mainly by the type of coal being burned and used combustion conditions [6]. The chemical compositions of investigated fly ashes and bottom ash are presented in Table 2. It is obvious that chemical composition of bottom ash is similar to the fly ash, but as expected contain higher content of unburned carbon. The present metal oxides are in the order: $\text{SiO}_2 > \text{Al}_2\text{O}_3 > \text{Fe}_2\text{O}_3 > \text{CaO} > \text{MgO} > \text{K}_2\text{O} > \text{Na}_2\text{O} > \text{TiO}_2$. The sum of $\text{SiO}_2 + \text{Al}_2\text{O}_3 + \text{Fe}_2\text{O}_3$ in fly ashes is higher

Fig. 3 Particle size distribution of BA**Table 1** Physical characteristics of the investigated coal ashes

Property	FA	LFA	BA
Specific surface area, ($\text{m}^2 \text{g}^{-1}$)	5.97	22.71	40.25
Moisture content, (wt. %)	1.36	4.42	4.46
Particle density, (g cm^{-3})	2.01	2.12	1.88
Bulk density, (kg dm^{-3})	573	684	582
D_{50} (μm)	30.57	42	120

than 70 wt.% and CaO content is lower (less than 10 wt.%) implies to fly ash F type i.e. siliceous ashes with pozzolanic properties [32, 33]. According to [34] FA belongs to type V (siliceous fly ash). The $\text{SiO}_2/\text{Al}_2\text{O}_3$ ratio predicts the potential reactivity of fly ash. It is 2.31 and 2.18 for FA and LFA, respectively i.e. in range of reported in [6].

Reactive SiO_2 in FA is 37.19 wt.%, which is in accordance to the one of the criteria FA to be used as SCM's (supplementary cementitious materials) in cement production. Reactive SiO_2 content shall not be less than 25 wt.% [34]. In cement production FA can be used as raw material for clinker production or as pozzolanic additive in blended cements. The content of FA has to be optimized due to the fact that FA has early low reactivity that influence on decrease of early strength. When FA is used as additive to Portland cement, particularly F type of fly ash, there are many positive effects on the resulting concrete, such as: lower water demand for similar workability when OPC is used; decrease of ratio water-cement and capillary porosity; enhance concrete workability and reduce bleeding [6]. Due to the similar chemical (composed mainly of SiO_2 , Al_2O_3 , Fe_2O_3 and CaO) FA and BA can be used as replacement of

clay in the brick production. The coarse particles influence on the plasticity index of clay and it can be used for decreasing of shrinkage in plastic clay.

An important parameter relating to the unburned carbon content is LOI (loss of ignition). As can be seen from Table 2, the highest value of LOI has BA (23.49 wt.%). According to [33] the fresh FA (LOI – 2.43%) belongs to group A (LOI < 5) while the higher content in the landfilled fly ash (LFA) is associated with the type of the used coal and the combustion condition in the past. As for the bottom ash (BA), the large percentage of loss of ignition may be an advantage over some applications that require a high coal content and thus a loss of ignition. Authors [6] described possibility of usage of ashes with higher content of LOI as low-cost adsorbent for gas and water treatment, particularly as adsorbent of sulphur compound, NOx adsorbent, removal of mercury, adsorbent of organic compounds or removal of metals from waste water.

Trace/Heavy Elements, Rear Earth Elements (REE) and other main elements are presented in Tables 2, 3, 4 and 5.

The elements of greatest concern, are As, Cd, Hg, Pb, Se as well as Zn, due to their potentially detrimental impact on human health and the environment. From the data presented in Table 3 especially the quantity of As, Cd, Co, Ch, Cu, Ni and V are much lower than reported in [35]. Also, it is evident (Tables 2, 3, 4 and 5) that the quantity of some of the trace elements in fly ash is much higher than bottom ash which corresponds to the ratio between bottom ash and fly ash in pulverized coal combustion plants. The concentration of trace elements in the ashes depends on several factors including the type of coal feed, coal source, the occurrence of significant elements and their association with the organic

Fig. 4 SEM/BSE microphotographs of the **a** FA, **b** LFA, **c** BA

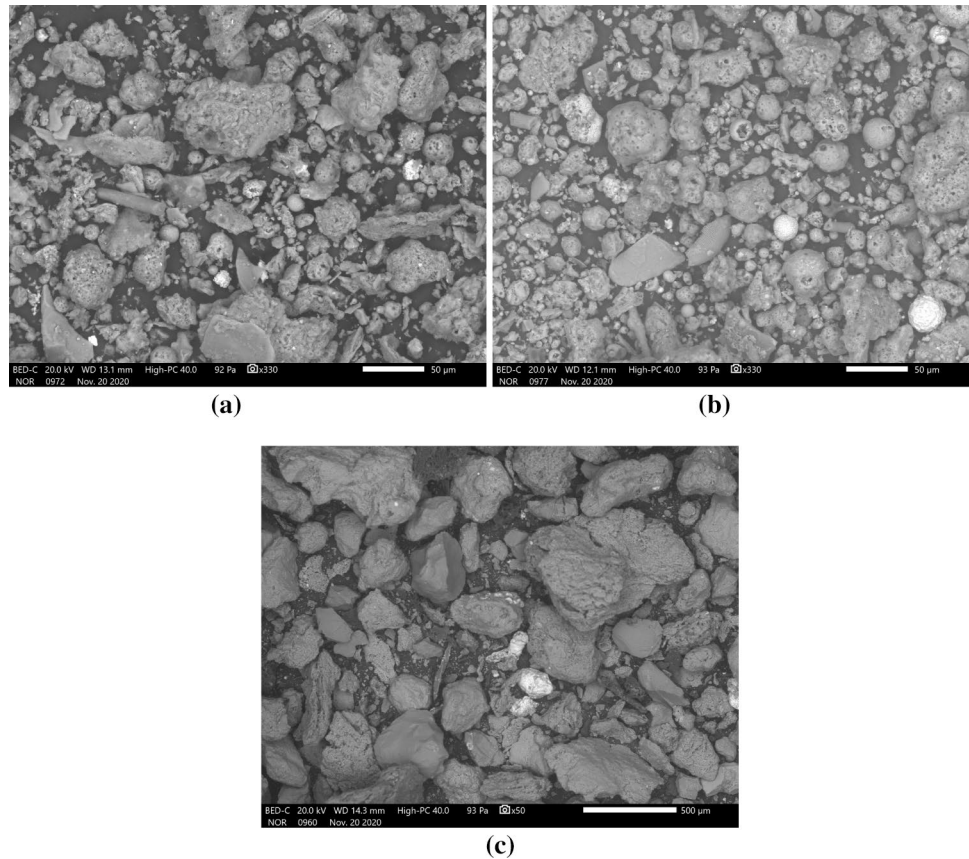


Table 2 Chemical composition of the investigated coal ashes

Ash	Chemical composition, wt. %												Σ
	LOI	SiO ₂	Reac SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	SO ₃	K ₂ O	Na ₂ O	P ₂ O ₅	TiO ₂	
FA	2.42	53.49	37.19	23.16	7.73	3.31	2.18	0.72	3.13	0.98	0.15	0.92	98.19
LFA	9.74	49.25	–	22.61	7.23	5.13	2.13	0.29	1.91	0.39	0.17	0.74	99.58
BA	23.49	48.47	–	15.67	5.01	1.77	1.22	0.19	2.14	0.59	0.09	0.52	99.16

and inorganic components of the coal, combustion conditions, volatilization-condensation mechanisms and the particle size of the ash. The fine ash particles, which have relatively larger surface areas, are in general enriched in trace elements [35]. Generally, most trace elements in coal ashes do not pose a threat when it is used for construction purposes. A previous study [36] confirms that leaching of trace elements from fly ash concrete was in the frame of the legal specifications. Concrete containing fly ash samples poses similar or higher trace element concentrations compared to Portland cement concrete. However, hazardous trace elements in ashes might pose environmental and public health risk. It is highly important to analyze the occurrence, distribution and mobility of trace elements for better management and possible remediation strategy. Liu et al. [37] found that low-mobility of trace elements (including Cr, Co, Cu, Ni,

Zn, Cd and Pb) in class F fly ash which might be a result of particle encapsulation by glass phase.

Besides certain heavy elements, coal fly ash also contains valuable rare earth elements (REE). Fresh fly ash contained < 380.8 ppm of REEs with a noteworthy ratio of heavy (Y, Eu, Gd, Tb, Dy, Ho, Er, Tm, Yb) to light (Sc, La, Ce, Pr, Sm) rare earth element (< 0.23). Taking into account the fact that ashes have no mining costs, the recovery of REEs could be potentially viable from the economic and environmental point of view.

Table 6 shows the content of amorphous and crystalline phases present in coal ashes. According to Blissett and Rowson [38] the mineralogy classification system divided four phase-mineral fly ash types namely Pozzolan (P), Inert (I), Active (A) and Mixed (M): this is based on the distinct behavior of (1) glass; (2) quartz and mullite; and (3) the sum of any other mineral-bearing phases such as

Table 3 Trace/Heavy elements in the investigated coal ashes

Parameter	Results (mg kg ⁻¹)		
	FA	LFA	BA
Trace/Heavy elements			
Pb	47 ± 9.4	23 ± 4.6	28 ± 5.6
As	50 ± 15	148 ± 44.4	< 20
Zn	150 ± 15	79 ± 7.9	75 ± 7.5
Co	19 ± 5.7	12 ± 3.6	6.6 ± 1.98
Cd	< 2	< 2	< 2
Cr	103 ± 10.3	82 ± 8.2	76 ± 7.6
Ni	66 ± 13.2	58 ± 11.6	39 ± 7.8
Sb	< 10	< 10	< 10
Mn	1333 ± 266.6	875 ± 175	1667 ± 333.4
Cu	130 ± 39	87 ± 26.1	34 ± 10.2
Ag	< 10	< 10	< 10
Ba	692 ± 69.2	506 ± 50.6	406 ± 40.6
Sr	300 ± 30	273 ± 27.3	149 ± 14.9
Ga	43 ± 21.5	39 ± 19.5	24 ± 12
Nb	24 ± 2.4	22 ± 2.2	14 ± 1.4
Ta	< 20	< 20	< 20
Th	34 ± 13.6	27 ± 10.8	18 ± 7.2
U	< 30	< 30	< 30
V	138 ± 27.6	115 ± 23	60 ± 12
Zr	125 ± 12.5	87 ± 8.7	50 ± 5
Hg	0.0097 ± 0.00	0.0364 ± 0.0083	0.0102 ± 0.0006

Table 4 REE elements in the investigated coal ashes

Parameter	Results (mg kg ⁻¹)		
	FA	LFA	BA
REE elements			
Ce	141 ± 14.1	130 ± 13	75 ± 7.5
Dy	7.1 ± 1.42	7.5 ± 1.5	< 5
Er	< 5	6.6 ± 2.64	< 5
Eu	< 3	< 3	< 3
Gd	< 10	11 ± 2.2	< 10
Ho	< 5	< 5	< 5
La	71 ± 7.1	51 ± 5.1	40 ± 4
Nd	57 ± 11.4	49 ± 9.8	28 ± 5.6
Pr	< 10	< 10	< 10
Sm	11 ± 2.2	12 ± 2.4	6.3 ± 1.26
Sc	13 ± 2.6	14 ± 2.8	7.0 ± 1.4
Tb	< 5	< 5	< 5
Tm	< 5	< 5	< 5
Yb	3.7 ± 0.74	4.7 ± 0.94	1.7 ± 0.34
Y	34 ± 6.8	35 ± 7	16 ± 3.2

**Lutetium was used as an internal standard, so it was not measured in the sample

Table 5 Be as another main element in the investigated coal ashes

Parameter	Results (mg kg ⁻¹)		
	FA	LFA	BA
Other main element			
Be	7.4 ± 0.74	5.2 ± 0.52	4.1 ± 0.41

Fe–Ca–Mg–K–Na–Ti–Mn oxides, hydroxides, sulfates, carbonates and silicates. Classifying fly ash in this way should help to simplify the choice of application for each unique fly ash composition.

Radiological characterization

Gamma-ray spectrometry

Table 7 presents the activity concentrations of ²²⁶Ra, ²³²Th and ⁴⁰K and I-index of examined fly ashes and bottom ash and the some typical values given for comparison.

Activity concentrations for ²²⁶Ra in the examined fly ashes and bottom ash are lower than EU typical and maximal values [39]. Also, ²²⁶Ra activity concentrations are lower than 207 Bq kg⁻¹ reported as an average activity concentration of this radionuclide for EU fly ashes [40]. The results are comparable with the ones reported in [41, 42]. It is noticeable that FA has significantly higher content of all measured radionuclides. The activity concentrations for ²³²Th are higher for both fly ashes than the reported values [43], but only FA has a higher ²³²Th activity concentration in relation to the value reported in [39, 42]. Regarding ⁴⁰K only FA has a higher content than the values reported in [39, 40]. As discussed in [43], the activity concentration is correlated to the fineness of the particles present in the material. The finer the particles, the higher the activity concentration, which can be clearly seen from the obtained results.

Regarding the I-index, only FA has value higher than 1 [44], but for the raw materials, it is only used as a screening tool. Fly ash can be used as a raw material in final building materials (like clinker, cement, concrete, brick, glass–ceramics, etc.) in certain mass portion (usually much lower than 100%). For example, in portland fly ash cement, a maximum of 35 wt.% of fly ash can be used [34]. Moreover, large number of samples analyzed in [43, 45, 46] showed that the final product (Portland cement and other building materials) had I lower than unity in all investigated samples which used FA as a component. Therefore the contribution of radionuclide content originating from the fly ash in these products is lower and the overall I-index for such products would be lower than 1.

Table 6 Content of amorphous and crystalline phases in coal ashes (wt. %)

Sample	Hematite	Illite/muscovite	Quartz	Plagioclase	K-feldspar	Dolomite	Amorphous
FA	0.5	9.8	8.7	13.7	–	0.1	67.2
LFA	1.1	-	6.2	16.1	–	0.1	76.5
BA	-	10.2	17.9	13.2	8.9	0.1	49.7

Table 7 Activity concentrations (Bq kg⁻¹) and I-index of ashes

Sample and literature referent value	Activity concentrations (Bq kg ⁻¹)			I- index
	²²⁶ Ra	²³² Th	⁴⁰ K	
FA	143 ± 7	116 ± 9	719 ± 50	1.30
LFA	83.5 ± 4	88 ± 6	383 ± 25	0.85
BA	69.5 ± 4	63 ± 6	457 ± 35	0.7
Typical activity concentration [39]	180	100	650	
Fly ash [40]	207	80	564	
Maximal activity concentration [39]	1100	300	1500	

Table 8 Calculated radium equivalent activity (Ra_{eq}), external hazards index (H_{ex}), external absorbed dose rate (D) and annual effective dose rate (EDR) for the ashes

Sample	Ra _{eq} (Bq kg ⁻¹)	H _{ex} (Bq kg ⁻¹)	D (nGy h ⁻¹)	EDR (mSv y ⁻¹)
FA	364.24	1.00	166.11	0.20
LFA	238.83	0.66	107.70	0.13
BA	194.78	0.54	89.22	0.11

Dose assessment & radium equivalent activity & The external hazard index

Radium equivalent activity (Ra_{eq}), external hazards index (H_{ex}), the external absorbed dose rate (D) and annual effective dose rate (EDR) were calculated in order to estimate a possible health effect due to the exposure of public to natural radionuclides present in the ashes, Table 8.

Ra_{eq} for all examined ashes is lower than 370 Bq kg⁻¹ which proves that the estimated hazard (gamma dose) associated with ashes containing ²²⁶Ra, ²³²Th and ⁴⁰K is under the limit of 1 mSv y⁻¹[31].

Another radiological criteria to estimate the suitability of materials, from the radiological point of view, is the external hazard index, H_{ex}, which value has to be < 1. The H_{ex} values for LFA and BA are lower than the limited one, but for FA the value is on the border of the prescribed limit, which is to be expected considering the relatively high value of Ra_{eq}.

The values for external absorbed dose rate, D, for examined ashes are higher than the estimated value of 60 nGy h⁻¹ for the population—weighted average in the outdoor air from terrestrial gamma radiation [44]. Sanjuán [47] reported the value of 141 nGy h⁻¹ for fly ash. It was used as a raw material in the CEM IV cement where the external absorbed dose rate was under the prescribed limits (39 nGy h⁻¹) due

to the use of a certain portion of fly ash in the final cement product. In [44] the reported external absorbed dose in the samples of Portland fly-ash cement and Portland-composite cement with FA ranged from 40.6 to 94.7 nGy h⁻¹. In pozzolanic Portland cement with siliceous FA, this value ranged from 66.3 to 176.6 nGy h⁻¹, while in the case of natural pozzolan cements, the external absorbed dose ranged from 57.3 to 101.9 nGy h⁻¹. According to this data, it is not expected that the addition of FA as a constituent of Portland cement would have a significant impact on the external absorbed dose originating from the final product.

The annual effective dose rate for all ashes is ≤ 0.2 mSv y⁻¹. The values are below the average global annual indoor absorbed dose rate in the air (0.41 mSv y⁻¹) from terrestrial sources of the radioactivity [48] and the effective dose rate threshold level of 1 mSv y⁻¹ given for the population by the European Basic Safety Standard [20]. This conclusion is in agreement with the conclusion regarding annual effective dose rate given in [44].

Higher values of Ra_{eq}, H_{ex}, D and EDR for FA are to be expected as all of these values are directly dependent on the activity concentration of ²²⁶Ra, ²³²Th and ⁴⁰K. Again, as it was shown in [43], the activity concentration of naturally occurring radionuclides is correlated to the grain size of the material and since the fly ash has the smallest grain size, it is expected to have the highest content of radionuclides and therefore the largest values of Ra_{eq}, H_{ex}, D and EDR.

Conclusions

In this study, fly ash (fresh and landfilled) and bottom ash from thermal power plant REK Bitola, Republic of North Macedonia have been characterized from physical, chemical

and radiological aspect. Based on the presented results and reviewed literature, the summary of the paper is as follows:

- The physical characteristics (specific surface area, moisture content, particle density and bulk density) of land-filled fly ash (LFA) is generally higher in comparison to the fly ash obtained from electro filter (FA). Bottom ash (BA) has higher specific surface area ($40.25 \text{ m}^2/\text{g}$) and lower particle density (1.88 g/cm^3) in relation to the both fly ashes, higher moisture content (4.46%) in relation to fly ash (1.3%) and possess coarser particles ($D_{50} = 120 \text{ }\mu\text{m}$) with irregular geometry in comparison to the both ashes.
- Relating to the chemical composition, fly ash belongs to siliceous ash with pozzolanic properties. The biggest content of unburned coal was detected in bottom ash resulting in high amount of LOI (23.49 wt. %). Relating to the trace/heavy elements, FA shows the highest values for most of them. The content of the most rare earth elements was lower in BA. Both fly ashes are characterized with high content of amorphous phase (more than 65%) and quartz and plagioclase are the dominant minerals in all investigated ashes.
- Based on the calculated doses and having in mind that the ash is used in certain portion in final product, the low impact from a radiological viewpoint can be concluded for all three examined ashes.

The examined ashes in this paper have the potential for utilization as secondary raw material in construction sector (cement, concrete, bricks, tiles, glass–ceramics, geothermal purposes....), but also the possibilities for their green transformation (carbon nanotubes, geopolymers, absorbents, rare earth elements, zeolites...) are foreseen. Anyway, more particular investigations have to be performed for utilizing fly ashes and bottom ash as secondary raw materials taking into account the purpose and the type of the final products.

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